

## Stability Balloon for Two-Dimensional Vortex Ripple Patterns

J. L. Hansen,<sup>1,2</sup> M. van Hecke,<sup>1</sup> C. Ellegaard,<sup>1</sup> K. H. Andersen,<sup>1,3</sup> T. Bohr,<sup>4</sup> A. Haaning,<sup>1</sup> and T. Sams<sup>2</sup>

<sup>1</sup>Niels Bohr Institute, Blegdamsvej 17, DK-2100 Copenhagen, Denmark

<sup>2</sup>Danish Defense Research Establishment, Ryvangs allé 1, Postbox 2715, DK-2100 Copenhagen, Denmark

<sup>3</sup>ISVA, Danish Technical University, Building 115, DK-2800 Kgs. Lyngby, Denmark

<sup>4</sup>Institute of Physics, Danish Technical University, Building 309, DK-2800 Kgs. Lyngby, Denmark

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Patterns of vortex ripples form when a sand bed is subjected to an oscillatory fluid flow. Here we describe experiments on the response of regular vortex ripple patterns to sudden changes of the driving amplitude  $a$  or frequency  $f$ . A sufficient decrease of  $f$  leads to a “freezing” of the pattern, while a sufficient increase of  $f$  leads to a *supercritical* secondary “pearling” instability. Sufficient changes in the amplitude  $a$  lead to *subcritical* secondary “doubling” and “bulging” instabilities. Our findings are summarized in a “stability balloon” for vortex ripple pattern formation.

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A flat bed of sand subjected to an oscillatory flow of water is seldom stable but instead displays the formation of patterns. Classical studies [1] have shown that, after the flat bed becomes linearly unstable, so-called rolling grain ripples (small heaps of grains) are formed first. These are, however, always transient [2], and eventually strongly nonlinear *vortex ripples* are formed in a coarsening-type process. These ripples have triangular crests with slopes roughly at the angle of repose, and the flow around the ripple crests is dominated by vortices that occur in the wake of the ripples. Together with the converging flow at the “upwind” side of the ripples, these vortices yield sand mass transport directed toward the crests of the ripples, which is balanced by sand avalanching down when the slopes grow too large. The wavelength of such ripple patterns is comparable to the amplitude of the fluid motion which sets the scale for the size of the separation bubbles [2–4]; this wavelength is substantially larger than the most unstable wavelength of a flat bed [5,6].

To characterize the vortex ripples, we have studied their *pattern forming* properties [7]. From this perspective, the system combines a number of unique features. First, the driving is anisotropic which results in alignment of the ripples perpendicular to the flow. This allows for studies in one-dimensional (1D) geometries [2,8], although our experiments indicate that instabilities of the ripples lead to intrinsically two-dimensional (2D) patterns. Second, typical ripple wavelengths are essentially independent of the system and grain dimensions and  $f$ , but scale with the driving amplitude  $a$  [2,3]. Finally, due to the strongly nonlinear character of the development, it has thus far not been possible to describe the pattern dynamics in terms of an “amplitude equation” [7].

Our setup consists of a tray of sand that is oscillated with amplitude  $a$  and frequency  $f$  in a tank of water, allowing us to study two-dimensional patterns. To probe the fully developed vortex ripples, we have studied their response to sudden changes of the control parameters  $a$  and  $f$ . Our findings lead to a “stability balloon” for vortex

ripple pattern formation shown in Fig. 1. First we study the amount of grain motion for patterns that have evolved “freely” from the flat bed and have a wavelength selected by the driving amplitude. This leads to the “freezing line” in Fig. 1 (and discussed in more detail in Fig. 3). In the second set of experiments, we study the response of regular patterns with initially *fixed* wavelengths to changes in  $f$  or  $a$ . We find that a secondary “pearling” instability (Fig. 4) occurs when the frequency is sufficiently increased, while secondary “doubling” and “bulging” (Fig. 5) instabilities occur when the amplitude  $a$  is decreased or increased,

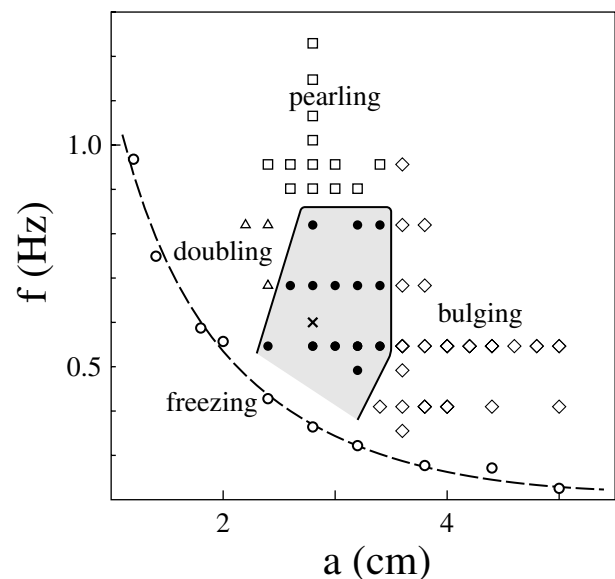


FIG. 1. Stability balloon for fully developed vortex ripples. The initial ripple pattern with wavelength 4.2 cm is compatible with driving parameters  $a = 2.8$  cm and  $f = 0.6$  Hz (cross) and remains stable for drivings indicated in full circles. Triangles, squares, and diamonds indicate drivings where this pattern experiences a doubling, pearling, or bulging instability. The open circles correspond to the  $n = 10$  measurements shown in Fig. 3 and the dashed line roughly indicates where the pattern freezes.

respectively, beyond some threshold. A qualitative presentation of these instabilities has appeared in [9].

*Experimental setup.*—Our setup is sketched in Fig. 2. An  $0.6 \text{ m} \times 1 \text{ m}$  aluminum tray (*A*) suspended from rollers (*B*) mounted on a stiff frame (*C*) is immersed in a sufficiently deep tank (*D*) filled with water. To avoid sloshing, a 3 cm thick flat plate of Plexiglas (*E*) is placed on top of the tank. The frame and tray are driven with a continuously controllable frequency  $f$  (period  $T$ ) and amplitude  $a$  by an ICME ac motor (*F*). The sides of the tray consist of 2 cm high straight boundaries, while the ends are triangular wedges with a slope of  $15^\circ$  and maximum height 2 cm (see Fig. 2); the rationale behind these “soft” boundaries will be discussed below. The “sand” consists of spherical glass beads, ranging in size from 250 to 350  $\mu\text{m}$ . The thickness of the sand layer is smallest in the troughs of the ripple pattern, but always larger than 5 mm. The whole setup is illuminated from the left side and filmed from above by a Dalsa 8-bit CAD4 CCD camera with  $1024^2$  resolution. A trigger is mounted on the motor so that all pictures are taken at the same extremal position of the tray. For the values of the driving considered here (Fig. 1), typical ripple patterns consist of 15–20 ripple lengths. Suspension can be ignored and the maximal acceleration of the tray is well below the fluidization threshold. For appropriate values of  $a$  and  $f$ , fairly regular ripple patterns grow from the flat bed. For example, for  $a = 2.8 \text{ cm}$  we find ripple patterns with wavelength 4.2 cm.

*Grain motion.*—Once a fully developed pattern is formed, how does the number of grains in motion vary with  $f$  and  $a$ ? We observed that, due to irregularities in some grains, sand bed images usually display a number of very bright spots. The difference between two subsequent images is dominated by the appearance or disappearance of a number  $N$  of such bright spots; we assume that  $N$  is proportional to the number of grains which have moved.

To measure  $N$  we proceed as follows: We start from a flat bed and obtain an equilibrated pattern by running the system for one hour, so that the driving amplitude selects the ripple wavelength, in contrast to the secondary instability experiments presented below. We then take a series 50 images from which the average of  $N$  is determined. The frequency is then lowered to a new value, the

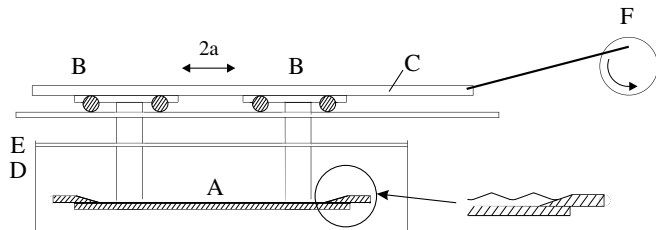


FIG. 2. Sketch of the experimental setup. The tray *A* is filled with sand and its oscillations are driven by the motor *F* via the rail *B*.

system is allowed to relax for 15 min, and 50 new images are recorded. This procedure is repeated for ten decreasing values of the frequency. In Fig. 3a, three examples of the number of moving grains as a function of frequency are shown. For large grain motions, suspension blurs the blinking grains and, consequently,  $N$  ceases to be a good measure for the grain motion: The corresponding data points were discarded in the analysis presented below.

The Shields parameter  $\sigma$  is a measure of the nondimensional shear stress on the sand bed and is defined as  $\tau/[gd(\rho_s - \rho_w)]$ , where  $\tau(x, t)$  is the shear stress on the bed,  $g$  denotes gravity,  $d$  is the diameter of the sand grains, and  $\rho_s$  and  $\rho_w$  are the densities of the sand and water. For fully developed vortex ripples,  $\sigma$  varies with space and time. Locally, the number of moving grains  $n$  is related to the Shields parameter as  $n \propto (\sigma - \sigma_c)$  when  $\sigma > \sigma_c$ ,  $\sigma_c$  being the threshold for grain motion [6]. What we measure is in fact  $N = \int dx \int dt n$ . Even though the variation of  $\sigma$  with space and time is not known in detail, we assume that this function scales with the maximum Shields parameter on a flat bed  $\sigma_m$ . As a result, we expect  $N$  to be an (unknown) function of  $\sigma_m$  only. For a laminar boundary layer, one obtains  $\sigma_m \propto af^{2/3}$  from the solution to Stokes’ second problem [10], while for turbulent flow a semiempirical relation  $\sigma_m \propto a^{1.75}f^2$  is appropriate [11]. In Fig. 3c we have plotted  $\sqrt{N}$  versus the turbulent expression  $a^{1.75}f^2$  and obtain a fairly good collapse, while the correlation between  $\sqrt{N}$  and the laminar expression  $af^{2/3}$  is very weak (Fig. 3d). This indicates that the sand transport is driven by a turbulent flow.

*Secondary instabilities.*—Thus far we have described patterns with a wavelength that is selected by the driving amplitude. Now we ask what happens when a perfectly

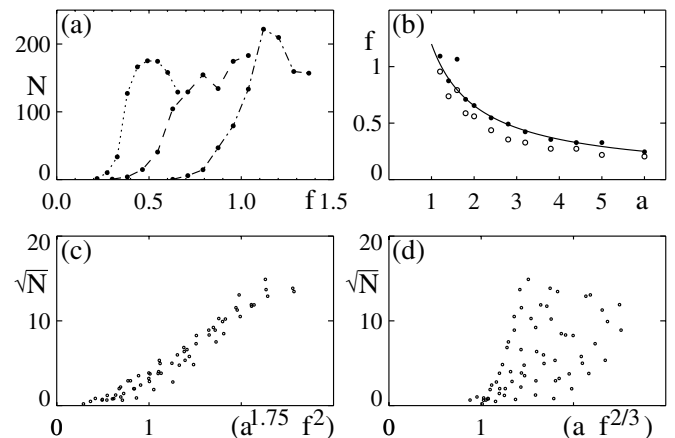


FIG. 3. (a) The average amount of moving grains  $N$  as a function of the driving frequency  $f$  for amplitudes 1.4 (dot-dashed), 2.4 (dashed), and 4.4 (dots). (b) Points in control parameter space where  $N$  is 10 (open circles) and 50 (closed circles) compared to a curve where  $a^{7/4}f^2$  is constant. (c) and (d) Data collapse of  $\sqrt{N}$  versus the turbulent expression  $a^{7/4}f^2$  and the laminar expression  $af^{2/3}$ , with  $a$  in cm and  $f$  in Hz (we have chosen  $\sqrt{N}$  for clarity).

regular pattern is suddenly subjected to changes in the driving parameters  $a$  or  $f$ .

Obtaining a completely regular pattern is not entirely trivial. Freely grown patterns contain defects, which may be annihilated only after long times (on the order of days), although other distortions of the pattern may then appear. These are partially driven by a small drift of the pattern, which has a velocity on the order of one ripple wavelength per  $10^4$  oscillations [12]. The deformations due to the drift are partly eliminated by using the slanted boundaries, allowing ripples to “drift out” of the system (leading to a small loss of sand at the edge of the plate). To obtain completely regular initial conditions, we have adopted the following procedure: First a flat bed is obtained by fluidizing the sand during a short period of strong oscillations of the plate. Then a regular pattern is imprinted into the sand by pressing down a frame with parallel equally spaced metal ridges. Small irregularities are then eliminated by a few ( $\approx 10$ ) oscillations of the plate.

By making large changes in  $a$  or  $f$  it is relatively simple to get regular secondary instability patterns as shown in Figs. 4 and 5. A study of the precise nature of these transitions involves runs performed at parameters close to the instability boundaries. Here time scales are long and the pattern is very sensitive to deformations due to drift, so it can be difficult to distinguish genuine instabilities from “experimental artifacts.” By introducing appropriate order parameters, we will below precisely characterize both the pearling and the bulging instability.

**Pearling.**—When the driving frequency is increased beyond a certain critical value, we find a secondary pearling instability (Fig. 4). Here, the crests of the initial ripples remain essentially undisturbed, but in their troughs

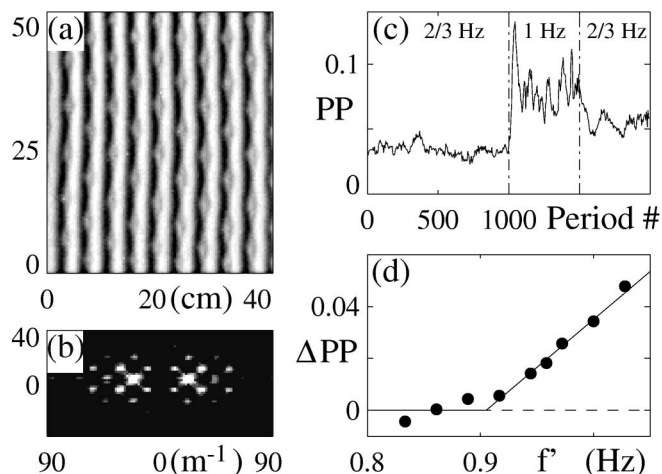


FIG. 4. (a) Central section ( $43 \text{ cm} \times 53 \text{ cm}$ ) of a pearling state obtained by subjecting a pattern with wavelength  $4.2 \text{ cm}$  to a driving of  $a = 2.8 \text{ cm}$  and  $f = 1 \text{ Hz}$ . (b) Corresponding power spectrum (range  $188 \text{ cm}^{-1} \times 94 \text{ cm}^{-1}$ ). (c) Time series of  $PP$  when  $f$  is changed from  $2/3 \text{ Hz}$  to  $f' = 1 \text{ Hz}$  and back again. (d) The order parameter  $\Delta PP$  as a function of the frequency  $f'$ . For details see text.

new small ripples (pearls) emerge, and the resulting stable pearling pattern is periodic with the pearls aligned on lines inclined by approximately  $45^\circ$ . The pearling transition is a *supercritical* secondary instability. When pearls are formed, their strength quickly saturates at some well defined value, and they disappear when the frequency is lowered as shown in Fig. 4c: Starting from an imprinted perfect ripple pattern with wavelength  $4.2 \text{ cm}$  (corresponding to an amplitude  $a = 2.8 \text{ cm}$ ), the system was driven at a low frequency of  $0.67 \text{ Hz}$ . After 1000 oscillations, the frequency was suddenly increased to  $f'$ , kept there for 500 oscillations, and then again lowered to the initial frequency.

To characterize the strength of the pearls, we have measured  $PP$ , the total intensity in the primary satellite peaks of the power spectrum (Fig. 4b). Because of finite size effects and noise,  $PP$  is not zero for perfect patterns, and as order parameter we therefore use  $\Delta PP$ , the difference between mean values of  $PP$  during period 1000–1500 and period 0–1000. A plot of  $\Delta PP$  as a function of the quenching frequency  $f'$  shows a well-defined transition point, above which the order parameter increases continuously (see Fig. 4d). A further increase of the frequency leads to more erratic states and finally to fluidization where the ripple patterns are washed away.

**Bulging.**—When the driving amplitude  $a$  is increased sufficiently, the regular ripple patterns become unstable to two-dimensional modulations. While we cannot completely rule out that this is a long wavelength instability [7], our data strongly suggests that the wavelength of this modulation perpendicular to the ripples is locked on 4 times the wavelength of the underlying pattern, with a similar wavelength along the ridge of the ripples. In contrast to the pearling instability, this instability is subcritical. The bulging deformations grow until neighboring ripples become so close that they form defects, which climb and glide rapidly through the system, finally leading to a regular pattern with a larger wavelength. For a sequence

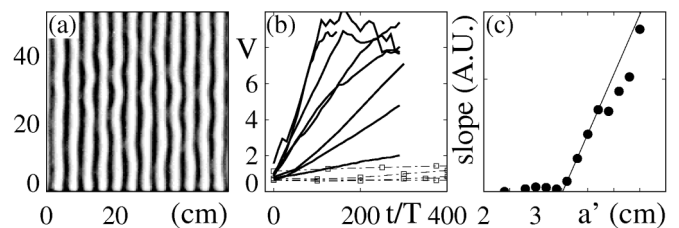


FIG. 5. (a) Central part ( $53 \text{ cm} \times 53 \text{ cm}$ ) of a bulging pattern, 525 T after the driving amplitude is changed to  $4 \text{ cm}$  ( $f = 0.41$ ). (b) The growth of deviations of a straight ripple pattern, quantified by the variance  $V$  for  $f = 0.55 \text{ Hz}$  and a range of amplitudes. The thin curves with symbols correspond to amplitudes  $2.4, 2.8, 3.0, 3.2,$  and  $3.4 \text{ cm}$  (below the bulging instability), while the thick curves correspond to  $3.6, 3.8, 4.0, 4.2, 4.4, 4.6, 4.8,$  and  $5.0 \text{ cm}$  (above the bulging instability). (c) The maximum slope of  $V$  (for times up to  $300T$ ) as a function of  $a$  shows a sharp transition for  $a \approx 3.55 \text{ cm}$ .

of pictures showing the development of the instability, see [9].

Close to the instability boundary, it becomes very difficult to distinguish slow drift from slow development of the instability, and we have therefore developed the following sensitive measure for the onset of the instability. Starting with a perfect pattern of wavelength 4.2 cm, we suddenly shift the amplitude. To characterize the time evolution of the pattern, we have extracted the local values of the ripple length  $\lambda_i$  taken over the whole two-dimensional image. The variance  $V$ , defined as  $\sum_{i=1}^N (\lambda_i - \bar{\lambda})^2 / (N - 1)$ , is then a simple measure for the amount of deformations in the pattern. The evolution of  $V$  is shown in Fig. 5b for a variety of values of the amplitude  $a$ .

Even below the formation of bulges,  $V$  grows slowly due to slow large scale deformations of the pattern, although the growth rate is essentially independent of the driving amplitude  $a$ . For  $a$  above some critical value,  $V$  displays a clear, surprisingly linear, growth after which saturation occurs for values of  $V$  of order 10. In Fig. 5c we have plotted the maximum of  $[V(tf + 100) - V(tf)]/100$  for  $t$  up to period 200. This quantity, which measures the maximum slope of  $V$ , clearly identifies the location of the secondary instability at  $a = 3.55(5)$  cm. In this way, we can distinguish between slow expansion or contraction of the pattern and the bulging instability.

*Doubling.*—When the amplitude  $a$  is decreased sufficiently, a subcritical *doubling* instability occurs. The initial phase of the development of this instability suggests that it can be captured in a one-dimensional framework. When the driving amplitude gets sufficiently small, the separation vortices that drive the sand transport no longer reach over the trough between ripples. This leads to the formation of bumps in the ripple troughs, which in turn grow out to form new ripples. Behavior similar to this has been seen in numerical studies of 1D vortex ripple patterns [4,13]. For a picture of this transition, see [9].

*Discussion and outlook.*—We have characterized some of the pattern forming properties of fully developed vortex ripple patterns. By observing the number of moving grains on the ripples, we have shown that the maximum shields parameter on the flat bed, calculated using the turbulent expression, is a relevant control parameter. We have shown that regular vortex ripple patterns are stable for a range of driving amplitudes and frequencies. Outside this range, the vortex ripples show a rich variety of secondary instabilities; pearling, bulging, and doubling.

Vortex ripples pose many theoretical challenges. The existence of a stable band and the doubling transition have been found in a simple model of ripple patterns [4].

The bulging and pearling are, to the best of our knowledge, not present in any simple theoretical models, such as Swift-Hohenberg-type models incorporating local mass conservation, left right symmetry, and a finite wavelength instability (which leads to spatial derivatives of order 6). We believe that the origin of the instabilities is basically hydrodynamical and related to the dynamics of the separation zones. In the doubling transition, it is thus clearly seen in the 1D experiments that the new ripples originate approximately at the reconnection point for the separation vortex. The bulging and pearling transitions are genuinely 2D and thus more complicated, but we speculate that the bulging transition is basically a Rayleigh-Plateau “sausage” instability of the almost cylindrical separation vortex, whereas the pearling instability might be related to the centrifugal instability of the cylinder, giving rise to transverse Taylor vortices. Obviously, these ideas need considerable elaboration in view of the strong time dependent shear experienced by the separation vortex.

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